

1) Paralelo na saída  $\Rightarrow$  Impedância  $\frac{Z}{1+A\beta}$

Logo  $Z_{Re} < Z \Rightarrow C //$

2) D

3) D

$$\begin{aligned}
 4) \quad T(e^{jT\omega}) &= 1 + 2e^{-jT\omega} + 3e^{-j2T\omega} + 3e^{-j3T\omega} + 2e^{-j4T\omega} + 1e^{-j5T\omega} = \\
 &= e^{-j2.5T\omega} (e^{j2.5T\omega} + e^{-j2.5T\omega} + 2e^{j1.5T\omega} + 2e^{-j1.5T\omega} + 3e^{j0.5T\omega} + 3e^{-j0.5T\omega}) = \\
 &= e^{-j2.5T\omega} (2\cos(2.5T\omega) + 4\cos(1.5T\omega) + 6\cos(0.5T\omega))
 \end{aligned}$$

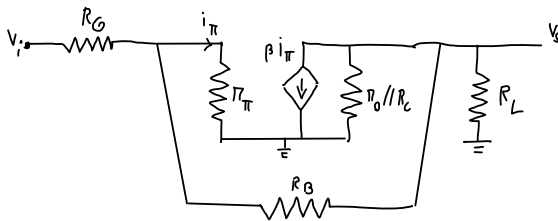
$$\phi = -2.5T\omega \quad A_{máx} = -\frac{\partial \phi}{\partial \omega} = 2.5T = \frac{2.5}{1M} = 2.5\mu s$$

D

5) B

II a) Paralelo - Paralelo  $\Rightarrow$  Transimpedância

b)



Matriz Y:

A

$$y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0} = \frac{1}{R_\pi}$$

$$y_{12} = \frac{I_1}{V_2} \Big|_{V_1=0} = 0$$

$$y_{21} = \frac{I_2}{V_1} \Big|_{V_2=0} = \frac{\beta}{R_\pi} = g_m$$

$$y_{22} = \frac{I_2}{V_2} \Big|_{V_1=0} = \frac{1}{R_L}$$

$$g_m = \frac{I_C}{V_T} = \frac{4mA}{25mV} = 0.16$$

$$A = \begin{bmatrix} \frac{0.16}{\beta} S & 0 \\ 0.16 S & 0.1mS \end{bmatrix}$$

$$\beta = \begin{bmatrix} 10 & -10 \\ -10 & 10 \end{bmatrix} \mu S$$

B

$$y_{11} = \frac{1}{R_B} \quad y_{12} = -\frac{1}{R_B}$$

$$y_{21} = -\frac{1}{R_B} \quad y_{22} = \frac{1}{R_B}$$

$$A^1 = -\frac{(0.16 - 10\mu)}{\left(\frac{0.16}{\beta} + 10\mu + \frac{1}{R_G}\right)\left(0.1m + 10\mu + \frac{1}{R_L}\right)} = -629.6K\Omega$$

$$B^1 = -10\mu S$$

$$K_V = \frac{A^1}{R_G} = \frac{A^1}{1+A^1\beta^1} \cdot \frac{1}{R_G} = -86.294 \Leftrightarrow$$

$$\Leftrightarrow R_G = \frac{A^1}{1+A^1\beta^1} \cdot \frac{1}{-86.294} = 1K\Omega \Leftrightarrow$$

$$\Leftrightarrow \frac{0.16}{\beta} = -\frac{(0.16 - 10\mu)}{\left(0.1m + 10\mu + \frac{1}{R_L}\right)} \cdot \frac{1}{A^1} - \frac{1}{R_G} - 10\mu \Leftrightarrow \beta = 800$$

c)  $A_0 = 140 \text{ dB}$

$\omega_{p1} = 2\pi \times 10^5 \text{ rad/s}$      $\omega_{p2} = 2\pi \times 10^7 \text{ rad/s}$

$A_f = 20 \text{ dB} = \frac{1}{\beta} \Leftrightarrow \beta = -20 \text{ dB}$

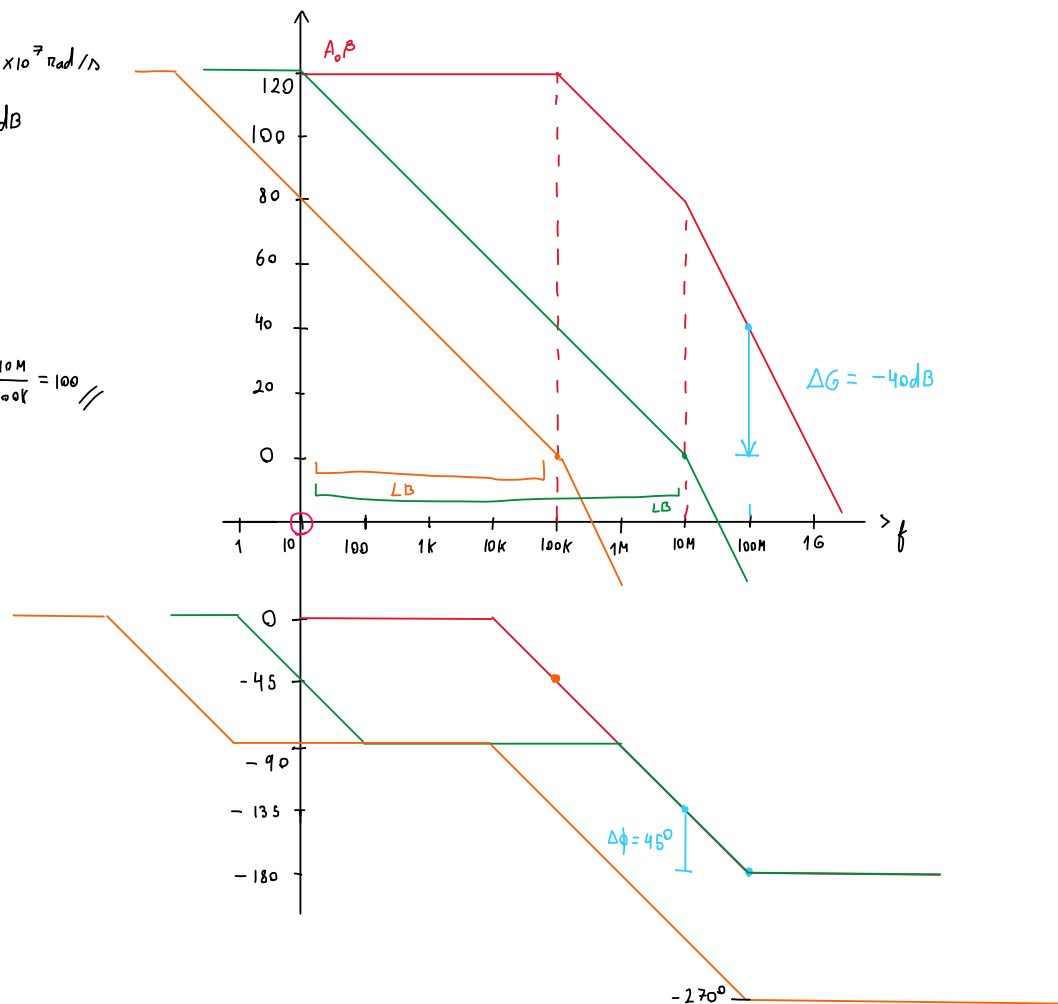
$A_0 \cdot \beta = 120 \text{ dB}$

Para  $f_{20} > 10 \text{ Hz}$

LB por deslocamento = 10M

LB por adição = 100k

$\alpha = \frac{10 \text{ M}}{100 \text{ k}} = 100 //$



III a) Passa-Banda

$A_p = 3 \text{ dB}$

$A_s = 20 \text{ dB}$

$\omega_{p1} = 800 \text{ Hz}$

$\omega_{s1} = 160 \text{ Hz}$

$\omega_{p2} = 1200 \text{ Hz}$

$\omega_{s2} = 4800 \text{ Hz}$

Queremos simetria  $\Rightarrow \omega_{p1} \times \omega_{p2} = \omega_{s1} \times \omega_{s2}$

$960 \text{ k} \neq 768 \text{ k}$

Logo temos de aumentar  $\omega_{s1} \Rightarrow \omega_{s1} = \frac{\omega_{p1} \times \omega_{p2}}{\omega_{s2}} = 200 \text{ k}$

$\Omega_s = \frac{\omega_{s2} - \omega_{s1}}{\omega_{p2} - \omega_{p1}} = 11.5$

$A_B(\Omega) = 10 \log(1 + \epsilon^2 \Omega^{2m})$

$A_B(1) = 3 \text{ dB} \Rightarrow 3 = 10 \log(1 + \epsilon^2) \Leftrightarrow \epsilon = 1$

$A_B(11.5) = 20 \text{ dB} \Rightarrow m = 1$

$H(s) = S + 1$

$T(\Omega) = \frac{1}{H(s)} \Big|_s = \frac{\Omega^2 + \omega_0^2}{B\Omega} = \frac{B\Omega}{\Omega^2 + \omega_0^2 + B\Omega} = \frac{B\Omega}{\Omega^2 + B\Omega + \omega_0^2} =$

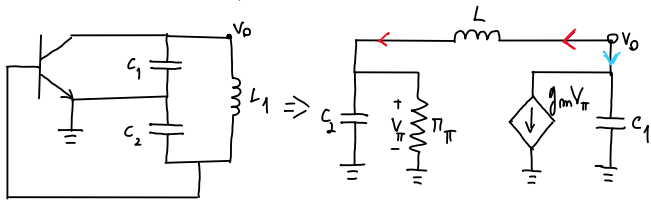
$\omega_0 = \sqrt{\omega_{p1} \times \omega_{p2}}$

$B = \omega_{p2} - \omega_{p1} = 400 \cdot 2\pi \text{ rad/s}$

$= \frac{2513\Omega}{\Omega^2 + 2513\Omega + 39.47 \times 10^6} //$

b) Para  $m=1$  as aproximações de Chebyshev e Butterworth não iguais //

c) Esquema simplificado:



$$\bullet \frac{V_{\pi}}{\left(\Delta C_2 + \frac{1}{\pi_{\pi}}\right)^{-1}}$$

$$V_0 = ? \Leftrightarrow V_0 - V_{\pi} = \Delta L \left( \frac{V_{\pi}}{\left(\Delta C_2 + \frac{1}{\pi_{\pi}}\right)^{-1}} \right) \Leftrightarrow$$

$$\Leftrightarrow V_0 = V_{\pi} \left( 1 + \Delta L \left( \Delta C_2 + \frac{1}{\pi_{\pi}} \right) \right)$$

$$\bullet g_m V_{\pi} + V_0 \Delta C_1$$

$$\text{Loop: } \frac{V_{\pi}}{\left(\Delta C_2 + \frac{1}{\pi_{\pi}}\right)^{-1}} + g_m V_{\pi} + V_{\pi} \left( 1 + \Delta L \left( \Delta C_2 + \frac{1}{\pi_{\pi}} \right) \right) \Delta C_1 = 0 \Leftrightarrow \Delta C_2 + \frac{1}{\pi_{\pi}} + g_m + \Delta C_1 + \Delta^2 C_1 L \left( \Delta C_2 + \frac{1}{\pi_{\pi}} \right) = 0$$

$$\text{Parte imaginária: } \omega C_2 + \omega C_1 - \omega^3 C_1 C_2 L = 0 \Leftrightarrow \omega^2 C_1 C_2 L = C_2 + C_1 \Leftrightarrow \omega = \sqrt{\frac{1}{L} \cdot \frac{C_2 + C_1}{C_1 C_2}} = 15.7 \times 10^3 \text{ rad/s} = 2.5 \text{ KHz}$$

$$\text{Parte real: } \frac{1}{\pi_{\pi}} + g_m - \omega^2 \frac{C_1 L}{\pi_{\pi}} = 0 \Leftrightarrow \frac{1}{\pi_{\pi}} + g_m - \frac{1}{C_1 C_2} \cdot \frac{C_2 + C_1}{\pi_{\pi}} = 0 \Leftrightarrow 1 + g_m \pi_{\pi} - \frac{C_2 + C_1}{C_2} = 0 \Leftrightarrow g_m \pi_{\pi} = \frac{C_1}{C_2} \text{ condição de equalização}$$

IV

Programar

a) Vantagens: - Entrada não liga a uma porta

- Menos hardware
- Menor área
- Menos atrasos

b) - Aplicar tensões elevadas no gate flutuante para aproximar cargas

- Isto aumenta o  $V_{GS}$ , logo não é como não houver transistor

Apagar

- Aplicar tensões muito negativas no gate flutuante para retirar cargas

Desvantagens: - Tensão de ruído LOW maior que zero

- Possíveis erros de transmissão
- Consumo estático não nulo