

1) The two-phase series capacitor buck converter shown in Fig. 1 operates in CCM at $f_{sw} = 1/T_s = 1\text{MHz}$. The switch driving waveforms are illustrated in Fig. 2.
a) Derive the DC voltage transfer function V_o/V_i as a function of D (assume the converter is lossless and the inductance values are matched (i.e. $L_a = L_b$)).
Assuming $V_i = 12\text{V}$, $V_o = 1.2\text{V}$, $P_o = 12\text{W}$:
b) calculate the average currents I_a and I_b .
c) Select the inductance values, L_a and L_b , such that the peak-to-peak current ripple is less than 20% of the average current.
d) Sketch a plot of the current flowing through C_1 as a function of time.
e) Select C_1 to ensure that the peak-to-peak voltage ripple is less than 0.3V .
f) Sketch a plot of the current flowing through L_a and L_b .
g) Calculate the peak-to-peak current ripple in C_0 .
h) Calculate the peak-to-peak output voltage ripple ($C_0 = 47\text{ }\mu\text{F}$, $\text{ESR} = 5\text{m}\Omega$).

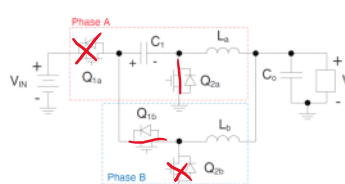


Fig. 1

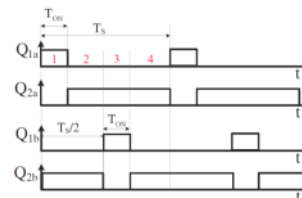
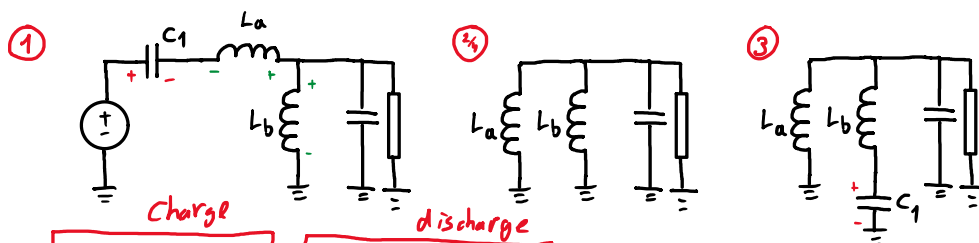


Fig. 2



a) $L_a \Rightarrow (V_o + V_{C1} - V_i)D + V_o(1-2D) + V_oD = 0$

$L_b \Rightarrow V_oD + V_o(1-2D) + (V_o - V_{C1})D = 0 \Rightarrow (V_o - V_i)D + V_o + V_o(1-2D) + V_o = 0 \Leftrightarrow \frac{V_o}{V_i} = \frac{D}{2}$
 $V_{C1} = V_o/D$

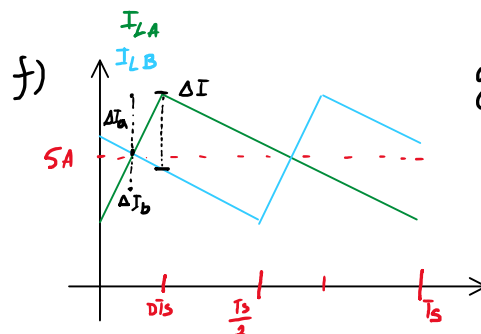
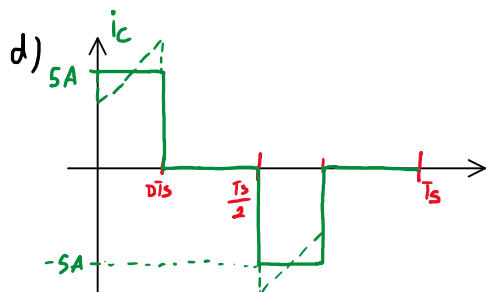
b) $V_i = 12\text{V}$ $2/4 \Rightarrow L_a = L_b \Rightarrow I_a = I_b$ and $I_a + I_b = I_o$

$V_o = 1.2\text{V}$ $I_a = I_b = \frac{I_o}{2} = 5\text{A}$

$P_o = 12\text{W}$

c) $L_a = L_b$ and $D = 0.2$

$\begin{cases} V = L_b \frac{\Delta i}{\Delta t} \\ \Delta i < 0.2 I_b \end{cases} \Rightarrow \frac{V_o D}{f_s L_b} < 0.2 I_b \Leftrightarrow L_b > \frac{V_o(1-D)}{0.2 I_b f_s} \Leftrightarrow L_b > 960\text{ mH}$



g) $\Delta I? \quad \frac{di}{dt} = \frac{V}{L}$

$\frac{\Delta I}{2} = \Delta I_a - \Delta I_b =$
 $= V_o \frac{(1-D)}{D L_a} \cdot \frac{D}{2} \cdot T_s - \frac{V_o}{L_b} \cdot \frac{D}{2} \cdot T_s =$

$\Delta I = \frac{V_o}{f_s} \cdot \frac{1-2D}{L} = 0.75\text{A}$

e) $i = C \frac{\Delta V}{\Delta t}$

$\Delta V < 0.3$

$C_1 \geq \frac{I D}{0.3 f_s} \Leftrightarrow C_1 \geq 3.33\text{ }\mu\text{F}$

h) $\Delta V_o = \Delta V_C + \Delta \text{ESR} = 4.75\text{ mV}$

$\Delta V_C = \frac{1}{2} \cdot \frac{T_s}{4} \cdot \frac{\Delta I}{2} \cdot \frac{1}{C} = \frac{\Delta I}{16 f_s C} \approx 1\text{ mV}$

$\Delta \text{ESR} = \Delta I \cdot \text{ESR} = 3.75\text{ mV}$

2) The DC/DC converter shown in Fig 3 operates in CCM.

a) Draw a plot of the DC voltage transfer function V_O/V_{IN} as a function of the duty cycle D and the turn ratio N_2/N_1 .

Given: $V_{IN} = 5 \text{ V}$, $V_O = 48 \text{ V}$, $P_O = 12 \text{ W}$; $f_{SW} = 500 \text{ kHz}$.

b) Select the turn ratio N_2/N_1 such that $D=50\%$.

c) Draw a plot of i_c and i_d as a function of time.

d) Select L_m such that the peak-to-peak current ripple is less than 10% of the average current.

e) Calculate L_m such that the peak-to-peak current ripple is less than 20% of the average current.

f) Select C_1 such that the peak-to-peak voltage ripple is less than 2% of the average capacitor voltage.

g) Select the filter capacitor C_o such that the peak-to-peak voltage ripple is less than 0.1% of the output voltage.

h) Determine the inductance factor of the magnetic core such that $N_1=5$ turns.

The tapped inductor is wound on a ferrite core having an effective volume of 0.628 cm^3 and an effective area of 0.3 cm^2 . The specific core loss can be approximated by the following expression, $P_{core} = C_m \cdot f^x \cdot B_{peak}^y$ [mW / cm³], where $C_m=2 \cdot 10^{-5}$, $x=1.8$ and $y=2.5$ (f in Hz and B in T).

i) Calculate the core loss.

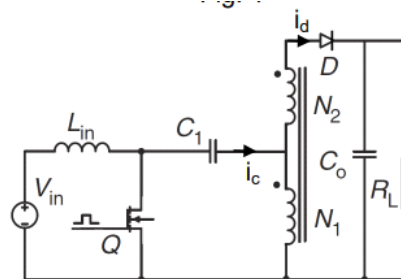
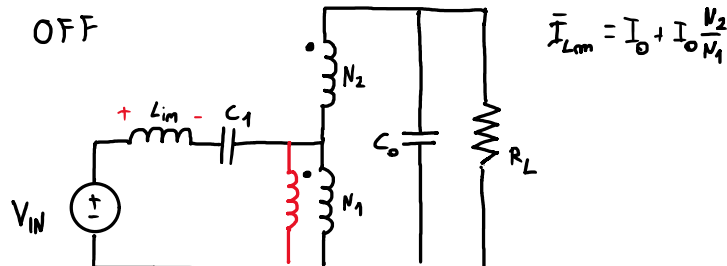
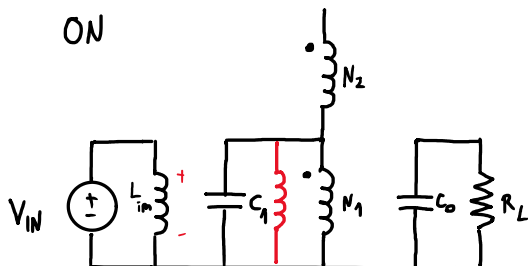


Fig. 3



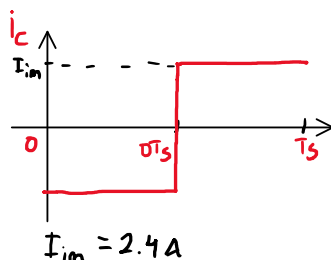
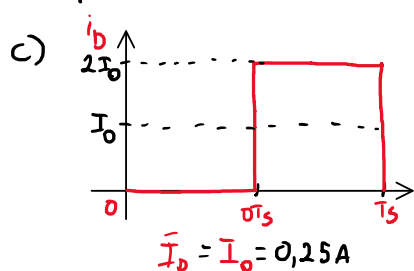
$$L_{im} \Rightarrow V_{im} D + (V_{im} - V_{C1} - \frac{V_O}{1 + \frac{N_2}{N_1}})(1-D) = 0 \Leftrightarrow$$

$$L_m \Rightarrow -V_{C1} D + \frac{V_O}{1 + \frac{N_2}{N_1}}(1-D) = 0 \Rightarrow \frac{V_O}{V_{IN}} = \frac{D}{1-D} \cdot (1 + \frac{N_2}{N_1})$$

$$h) L_m = N_1^2 A_L$$

$$A_L = \frac{L_m}{N_1^2} = 416 \text{ mH}$$

$$b) \frac{N_2}{N_1} = 8.6$$



$$i) L_m \Delta i = N_1 A_e \Delta B$$

$$\Delta B = \frac{L_m \Delta i}{N_1 A_e} = 33.28 \text{ mT}$$

$$B_{peak} = \frac{\Delta B}{2} = 16.64 \text{ mT}$$

$$P_{core} = P_c \cdot V_c = C_m \cdot f^x \cdot B^y \cdot V_c = 8.13 \text{ mW}$$

$$d) V = L \frac{\Delta I}{\Delta t} \Leftrightarrow \frac{V_{im} D}{f_s L_{im}} \leq 0.1 \cdot I_{im} \Leftrightarrow L_{im} \geq \frac{V_{im} D}{0.1 I_{im} f_s} \Leftrightarrow L_{im} \geq 20.8 \mu\text{H}$$

$$e) \bar{I}_{Lm} = I_O + I_O \frac{N_2}{N_1} \Rightarrow \frac{V_O(1-D)}{(1 + \frac{N_2}{N_1}) f_s L_m} \leq 0.2 \cdot I_O (1 + \frac{N_2}{N_1}) \Leftrightarrow L_m \geq \frac{V_O(1-D)}{0.2 \cdot I_O \cdot (1 + \frac{N_2}{N_1})^2 f_s} \Leftrightarrow L_m \geq 10.4 \mu\text{H}$$

$$f) I = C \frac{\Delta V}{\Delta t} \quad \Delta V \leq \frac{2}{100} \cdot V$$

$$V_{C1} = -V_{im} \quad \frac{I_{im}(1-D)}{f_s \cdot C} \leq \frac{2}{100} \cdot V_{im} \Leftrightarrow C \geq \frac{I_{im}(1-D)}{\frac{2}{100} \cdot f_s \cdot V_{im}} \Leftrightarrow C_1 \geq 24 \mu\text{F}$$

$$g) \frac{I_O \cdot D}{f_s \cdot C} \leq \frac{0.1}{100} V_O \Leftrightarrow C_O \geq \frac{I_O D}{\frac{0.1}{100} f_s V_O} \Leftrightarrow C_O \geq 5.2 \mu\text{F}$$