

1) The current-fed push-pull converter shown in Fig. 1 is operating at $f_{sw}=500$ kHz (assume ideal switches, diodes and transformer).

a) Derive the DC transfer function $\frac{V_o}{I_{IN}}$ assuming $n_1=n_2$.

Consider the following specifications: $I_{IN} = 5A$, $V_o=5 V$, $P_o = 10 W$.

b) Calculate the duty-cycle D.

c) Sketch a plot of the current i_d as a function of time.

d) Calculate the peak-to-peak output voltage ripple ($C = 470 \mu F$, ESR = $10 m\Omega$).

e) Derive the transfer functions $G_{oc}(s) = \frac{\tilde{V}_o}{\tilde{I}_d}$, assuming $G_{PWM}(s)=1 V^{-1}$ (**hint:** perturb and linearize the average diode current $\langle i_d \rangle_{T_s}$). Sketch the Bode plot of $G_{oc}(s)$.

f) Determine the compensator transfer function, $G_c(s)$, such that the loop gain has a constant slope of -20 dB / dec, crossing the 0dB axis at $f_c = 50$ kHz.

g) Sketch the asymptotic plot of the closed-loop output impedance.

h) Sketch the transient response to a load step of 0.5A.

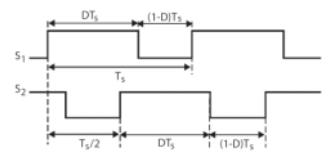
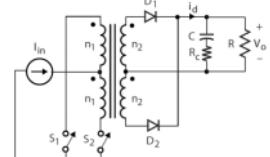
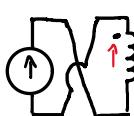
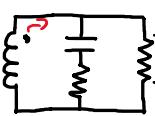


Fig. 1

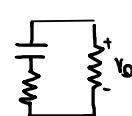
a) $S1 ON$
 $S2 OFF$



$S1 OFF$
 $S2 ON$



$S1 ON$
 $S2 ON$

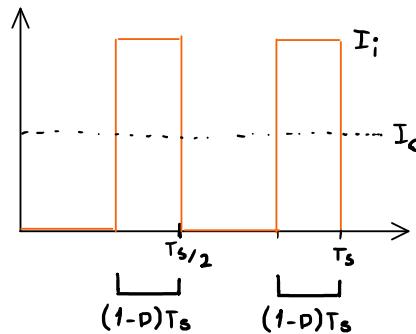
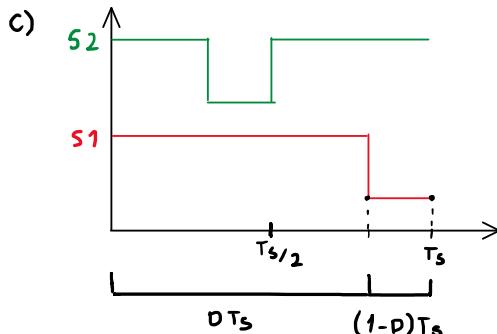


$$I_d = I_o = \frac{I_i(1-D)T_s + I_i(1-D)T_s}{T_s} \Leftrightarrow \frac{V_o}{R} = 2I_i(1-D) \Leftrightarrow \frac{V_o}{I_i} = 2R(1-D)$$

b) $I_i = 5A$

$$\begin{aligned} V_o &= 5V \\ P &= 10W \end{aligned} \Rightarrow \frac{V_o}{2 \cdot R \cdot I_i} = D = 0.8$$

$$R = 2.5 \Omega$$



d)

$$\Delta V_o = \Delta V_C + \Delta ESR = 52.55mV$$

$$\Delta ESR = ESR \cdot \Delta I = 50mV$$

$$I = c \frac{\Delta V}{\Delta t} \Rightarrow \Delta V_C = \frac{(I_{im} - I_o)(1-D)}{f_s \cdot C} = 2.55mV$$

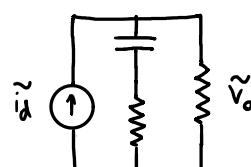
e) $I_d = 2I_i(1-D)$

$$\tilde{I}_d = \tilde{i}_d = 2(I_i + \tilde{i}_i)(1-D-\tilde{d})$$

$$\tilde{I}_d = 2I_i(1-D)$$

$$\tilde{i}_d = 2\tilde{i}_i(1-D) - 2I_i\tilde{d}$$

$$\frac{\tilde{i}_d}{\tilde{d}} = -2I_i \Leftrightarrow \frac{\tilde{V}_o}{\tilde{d}} = -2I_i \frac{R(1+DR_cC)}{1+DC(R+R_c)}$$



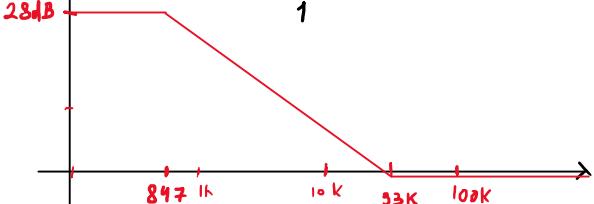
$$\frac{\tilde{V}_o}{\tilde{I}_d} = \frac{R(1+DR_cC)}{1+DC(R+R_c)}$$

$$G_{oc} = \frac{\tilde{V}_o}{\tilde{d}} \cdot \frac{\tilde{d}}{\tilde{V}_c} = -2I_i \frac{R(1+DR_cC)}{1+DC(R+R_c)}$$

$$|G_{oc}(s)| = 2I_i R = 25 \text{ dB}$$

$$\omega_z = \frac{1}{R_c C} = 212 \text{ rad/s} = 33.9 \text{ kHz}$$

$$\omega_p = \frac{1}{C(R+R_c)} = 847 \text{ rad/s} = 135 \text{ Hz}$$



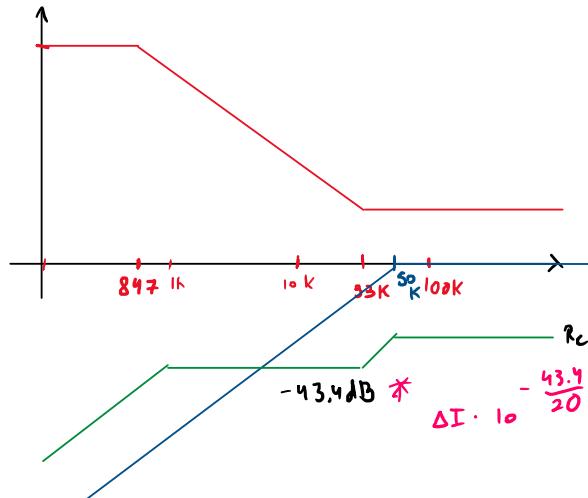
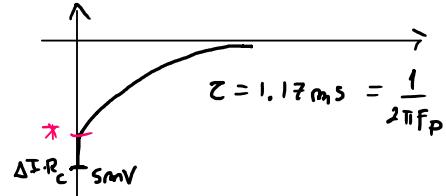
$$G_{oc} = -2I_i \frac{R(1+\Delta R_c C)}{1+\Delta C(R+R_c)} \quad L = \frac{\omega_c}{\Delta} \Rightarrow \frac{1}{1+L} = \frac{1}{1 + \frac{\omega_c}{\Delta}} = \frac{\Delta/\omega_c}{\Delta/\omega_c + 1}$$

$$L = G_{oc} \cdot G_C \quad G_C = \frac{L}{G_{oc}} = \frac{1}{2I_i} \cdot \frac{\omega_c}{\Delta} \cdot \frac{1+\Delta C(R+R_c)}{R(1+\Delta R_c C)}$$

g) $Z_{oc1} = \frac{Z_0 \Delta I}{1+L}$

h) $I_{Load} = 0.5 A$

$$Z_{oc1} = R // (R_c + \frac{1}{\Delta C}) = \frac{R(1+\Delta R_c C)}{1+\Delta C(R+R_c)}$$



2) The Cuk converter in Fig. 2 operates in CCM at $f_{sw}=250$ kHz. Consider the following specifications: $V_{IN}=12V$, $V_O=12 V$, $P_o=60 W$; $L_1=54 \mu H$; $L_2=27 \mu H$; $C_1=22 \mu F$; $C_2=100 \mu F$. Ripples are small.

a) Derive the DC voltage transfer function V_O/V_{IN} .

b) Calculate the average inductor currents I_{L1} and I_{L2} .

c) Calculate the peak-to-peak voltage ripple across C_1 .

The output resistor is increased, pushing the converter toward the CCM/DCM boundary:

d) Sketch a plot of i_D as a function of time at the CCM/DCM boundary (that is, $i_D(T_S)=0$).

e) Calculate the boundary output power.

f) Show that the converter operates in DCM for $K < K_{crit}(D)$, where

$$K = \frac{2 \cdot L_1 // L_2}{R \cdot T_S} \quad \text{and} \quad K_{crit} = (1-D)^2$$

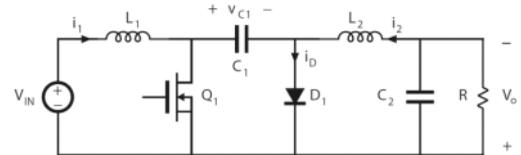
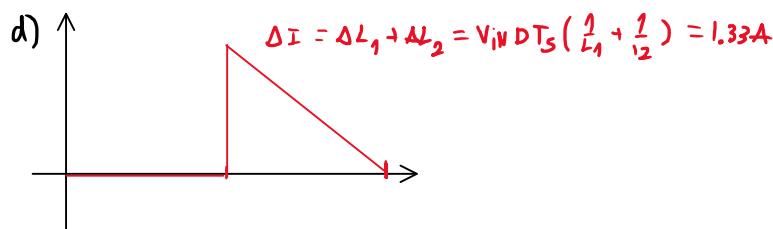


Fig. 2

a) $L_1: V_{IN}D + (V_{IN}-V_{C1})(1-D) = 0 \Leftrightarrow V_{IN} = \frac{V_O(1-D)}{D} \Leftrightarrow \frac{V_O}{V_{IN}} = \frac{D}{1-D} \Rightarrow D=0.5$
 $L_2: (V_{C1}-V_O)D - V_O(1-D) = 0 \Leftrightarrow V_{C1} = \frac{V_O}{D}$

b) $\bar{I}_{L1} = I_{im} = 5A \quad c) i = C \frac{dv}{dt} \Leftrightarrow \Delta V_{C1} = \frac{I_{im}(1-D)T_S}{C_1} = 0.45V$

$\bar{I}_{L2} = I_{out} = 5A$



e) $P_o = P_{L1} + P_{L2} = (L_1 \cdot \Delta I_{L1}^2 + L_2 \cdot \Delta I_{L2}^2) \frac{f_{sw}}{2} = \left(\frac{V_{im}^2 D^2}{f_s L_1} + \frac{V_{im}^2 D^2}{f_s L_2} \right) \frac{f_{sw}}{2} = \frac{V_{im}^2 D^2}{f_s 2} \cdot \left(\frac{1}{L_1} + \frac{1}{L_2} \right) = 4W!$

f) $\frac{V_{im} D}{2f_s L_1} + \frac{V_O(1-D)}{2f_s L_2} \geq \frac{P_o}{V_O} + \frac{P_o}{V_{im}} \Leftrightarrow \frac{V_O(1-D)}{f_s(L_1//L_2)} \geq \frac{V_O}{R(1-D)} \Leftrightarrow (1-D)^2 \geq \frac{2(L_1//L_2)}{R T_S}$