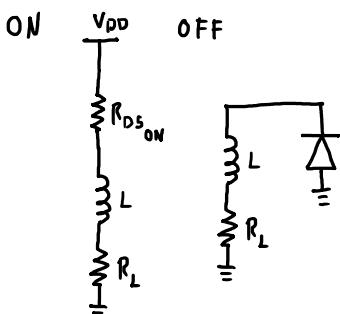


1) The high-side switch shown in Figure 1 is used to drive an inductive load. The load current is set to a value of 5A by a controller operating at a fixed frequency of 100 kHz ($R = 100 \Omega$, $R_L = 2 \Omega$, $L = 1 \text{ mH}$, $f_{\text{sw}} = 0.25 \text{ ms}$, $V_{\text{aux}} = 0 \rightarrow 5V$). The output characteristics of T1 are shown in Fig. 2).

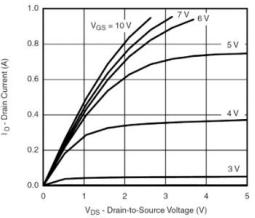
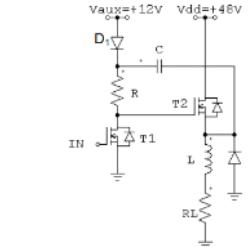
a) Calculate the duty cycle of the power MOSFET and the peak-to-peak ripple in the load current.

a) Volt second balance \Rightarrow $0 = [V_{\text{DD}} - (R_{\text{DS,ON}} + R_L) I_L] D - R_L I_L (1-D) \Leftrightarrow$
 $\Leftrightarrow D = \frac{R_L I_L}{V_{\text{DD}} - R_{\text{DS,ON}} I_L} = 21.4\%$



$$V_L = L \frac{di}{dt} \Rightarrow \frac{di}{dt} = \frac{V_L}{L}$$

$$\Delta i_L = \frac{[V_{\text{DD}} - (R_{\text{DS,ON}} + R_L) I_L] D}{L f_{\text{sw}}} = \frac{R_L I_L (1-D)}{L f_{\text{sw}}} = 78.6 \text{ mA}$$



b) Select the bootstrap capacitor C_B such that the maximum voltage drop, ΔV_{CB} is 500 mV (D1 has a leakage current of $2 \mu\text{A}$ and a Q_{RR} of 1 nC).

b) $\Delta V_{CB} = 500 \text{ mV}$ $\Delta Q_{CB} = C_B \cdot \Delta V_{CB}$

$$D_1 \Rightarrow \begin{cases} I_{\text{leak}} = 2 \mu\text{A} \\ Q_{RR} = 1 \text{ nC} \end{cases} C_B > \frac{Q_G + Q_{RR} + I_{\text{leak}} \cdot \frac{1}{f_{\text{sw}}}}{\Delta V_{CB}} \Leftrightarrow C > 26 \text{ mF!}$$

$$Q_G = C_{iss} \cdot V_{GS,\text{Max}} = 1000 \text{ pF} \cdot 12 \text{ V} = 12 \text{ mC}$$

c) Using the curves in Figures 3 and 4, calculate the average switching loss in the power MOS transistor ($V_{\text{th}} = 2.5 \text{ V}$).

Turn on: $T_1 \text{ OFF}$ [Let's assume $V_{D1} = 1 \text{ V}$]

$$V_{GSP} = 6.8 \text{ V} \quad V_B = V_{\text{aux}} - V_D = 11 \text{ V} \quad Q_2 = 5.2 \text{ mC}$$

$$t_{d_{\text{on}}} = 40 \text{ ms} \quad t_r = 12.4 \text{ ms} \quad t_{th} = 11 \text{ ms}$$

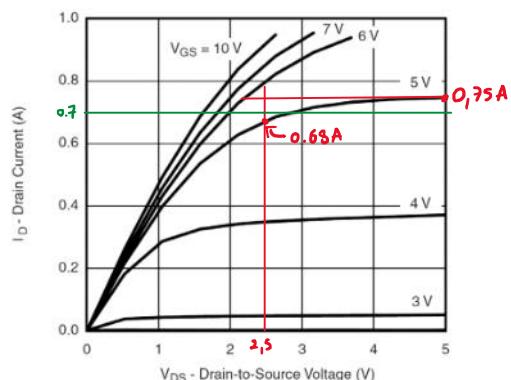
$$-t_{d_{\text{on}}} : V = V_{\text{DD}} + (V_B - V_{\text{DD}}) e^{-t_{d_{\text{on}}}/z} \quad z = RC_{iss} \quad C_{iss} = 420 \text{ pF}$$

$$-t_{d_{\text{on}}} : I_m \left(1 - \frac{V_{GSP}}{V_B} \right) \cdot RC_{iss} = t_{d_{\text{on}}} \Leftrightarrow t_{d_{\text{on}}} = R C_{iss} \ln \left(\frac{V_B}{V_B - V_{GSP}} \right) = 40 \text{ ms}$$

$$-t_r : t_r = \frac{Q_2}{I_{\text{driver}}} = \frac{Q_2 R}{V_B - V_{GSP}} = 12.4 \text{ ms} \quad -t_{th} : t_{th} = R C_{iss} \ln \left(\frac{V_B}{V_B - V_{th}} \right) = 11 \text{ ms} \Leftrightarrow \text{Relevant}$$

$$I_{\text{driver}} = \frac{V_B - V_{GSP}}{R}$$

Turn off: $V_{th} = 2.5 \Rightarrow V_{DS,\text{min},1} = V_{th} = 2.5 \text{ V}$



Plateau: t_f

$$I_{T_1} = 750 \text{ mA}$$

$$I_R = \frac{V_B - V_{GSP}}{R} = 43 \text{ mA}$$

$$I_{\text{sink}} = I_{T_1} - I_R = 707 \text{ mA}$$

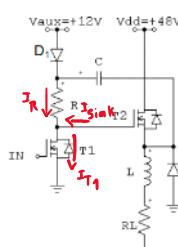
$$t_f = \frac{Q_2}{I_{\text{sink}}} = 7.4 \text{ ms}$$

Discharge: t_{dis}

$$I_{T_1,\text{min}} = 680 \text{ mA}$$

$$I_{R,\text{max}} = \frac{V_B - V_{th}}{R} = 85 \text{ mA}$$

$$I_{\text{sink},\text{min}} = 595 \text{ mA}$$



Assume $I_{\text{sink},\text{min}}$ for all $t \Rightarrow$ overestimate!

$$t_{dis} = \frac{Q_{aux}}{I_{\text{sink},\text{min}}} = 3.4 \text{ ms}$$

$$\begin{aligned} t_f &= 7.4 \text{ ms} & t_{d_{on}} &= 40 \text{ ms} \\ t_{dis} &= 3.4 \text{ ms} & t_r &= 124 \text{ ms} \\ t_{th} &= 11 \text{ ms} \end{aligned}$$

$$\begin{aligned} E_{ON} &= \frac{V_{DD} \cdot I_L}{2} (t_{d_{on}} + t_r - t_{th}) \\ E_{OFF} &= \frac{V_{DD} \cdot I_L}{2} (t_{dis} + t_f) \end{aligned} \quad P = \frac{V_{DD} \cdot I_L}{2} \cdot (t_{d_{on}} + t_r - t_{th} + t_{dis} + t_f) \cdot f_{sw} = 1.96 \text{ W} \approx 2 \text{ W}$$

d) Calculate the average power dissipation in the resistor R.

$$\text{If ON} \Rightarrow I_R = \frac{V_{aux} - V_{D_1}}{R} \quad P = (V_{aux} - V_{D_1})^2 / R \quad (1 - D) = 950 \text{ mW}$$

$$\text{If OFF} \Rightarrow I_R = 0$$

Assuming ideal transients since $t_s \gg t_{on/off}$

- 2) The inductive load of Fig.5 is driven by a MOSFET M1. $V_S = 15 \text{ V}$, $V_Z = 47 \text{ V}$, $L = 6 \text{ mH}$, $R_L = 3 \Omega$, $R = 100 \Omega$, $r_{DSonM1} \ll R_L$.

After the load current has reached the steady state value, the MOSFET M1 is switched off.

- a) Calculate the current flowing through the DMOS M2, whose output characteristics are shown in Fig. 6, after M1 is switched off.

a) At steady state $I_L(0) = 5 \text{ A}$

At turn-off

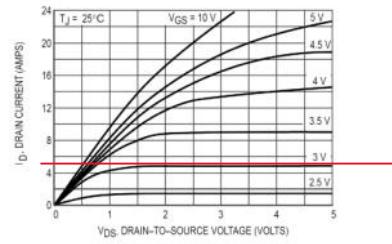
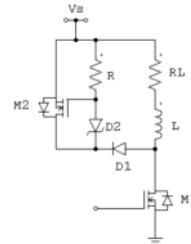
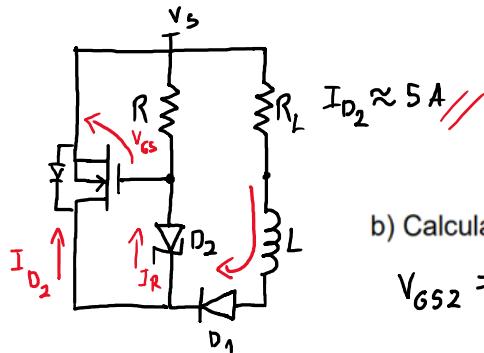


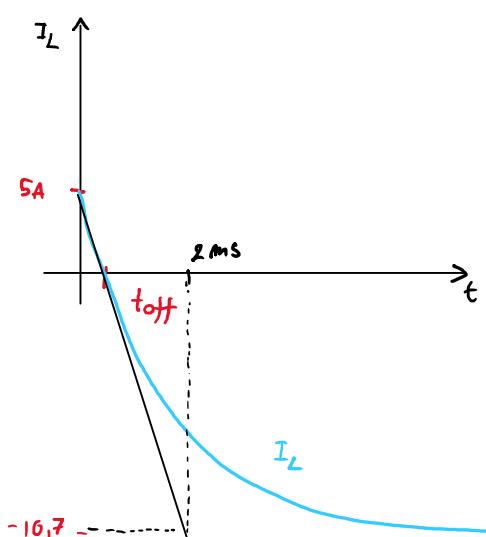
Fig. 5

Fig. 6

- b) Calculate the current flowing through the zener diode D2 after M1 is switched off.

$$V_{GS2} = 3 \text{ V} \quad V_R = 3 \text{ V} \Rightarrow I_R = I_Z = \frac{V_R}{R} = 30 \text{ mA}$$

- c) Draw a plot of the inductor current as a function of time. $\zeta = \frac{L}{R} = 2 \text{ ms}$



$$\begin{aligned} i_L(0) &= 5 \text{ A} \\ i_L(\infty) &= -\frac{V_{GS} + V_Z}{R_L} = -16.7 \text{ A} \end{aligned}$$

$$K_1 = i_L(\infty) = -16.7 \text{ A}$$

$$K_2 = i_L(0) - K_1 = 21.7 \text{ A}$$

$$I_L(t) = -16.7 + 21.7 e^{-t/\zeta}$$

$$\hookrightarrow t_{off} = t|_{i_L(t)=0} \Rightarrow \ln\left(\frac{21.7}{16.7}\right)\zeta = t = 0.524 \text{ ms}$$

$$I_L(t) = K_1 + K_2 e^{-t/\zeta}$$

$$I_L(0) = K_1$$

- d) Calculate the energy dissipated in the MOSFET M2 during the turn-off transient.

With ideal D1

$$V_{DS} = V_{GS} + V_Z = 50 \text{ V}$$

$$E = 50 \cdot \int i_L dt \approx 50 \cdot \frac{t_{off} \cdot I_L(0)}{2} = 65 \text{ mJ}$$