

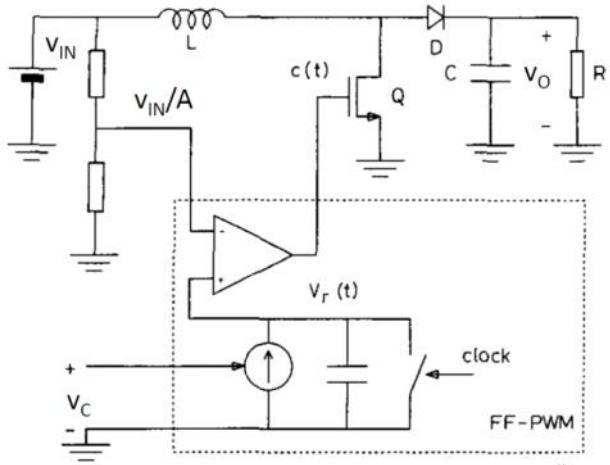
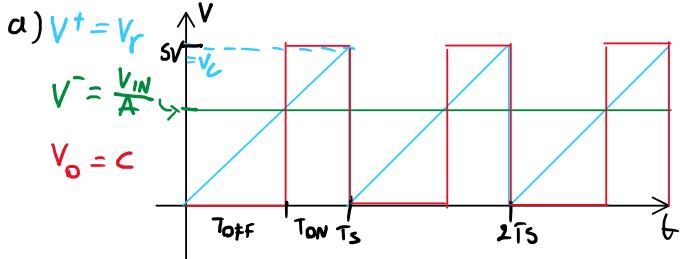
1) A boost converter with feedforward pulse-width modulator is shown in Fig 1. The converter operates in CCM. A sawtooth waveform $v_r(t)$ is obtained using an integrator with reset. A clock signal resets the integrator periodically with period T_s . The capacitor charging current in the integrator is proportional to the slowly-varying modulating input v_c . The periodic sawtooth waveform $v_r(t)$ is given by

$$v_r(t) = v_c \cdot \frac{t}{T_s}; \quad v_r(t + kT_s) = v_r(t)$$

$v_r(t)$ is compared with the scaled input voltage V_{IN}/A . The output of the comparator is the pulsating signal $c(t)$ that controls the switching transistor Q.

Given the following specifications: $V_{IN} = 35V$, $V_O = 50V$, $f_s = 100\text{ kHz}$, $V_C = 5V$:

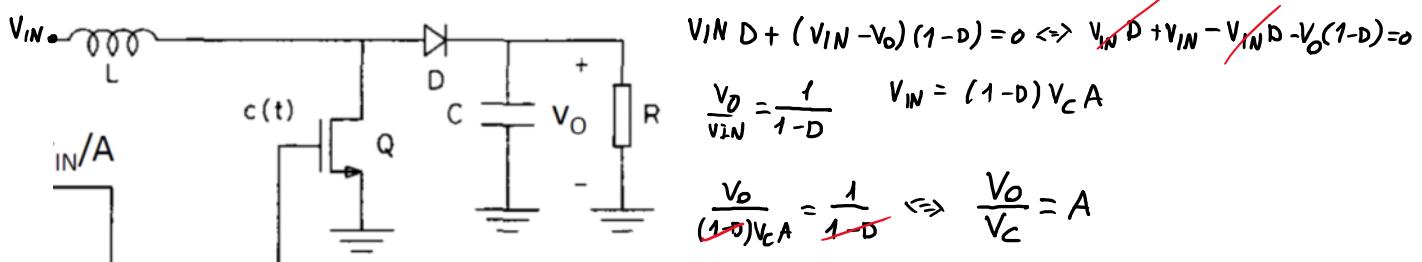
a) draw a plot of the voltage waveforms at the input and output of the comparator.



b) Derive the expression of D as a function of V_{IN} and V_C .

c) Derive the expression of the DC voltage transfer function V_O/V_C .

$$\frac{T_{OFF}}{V_{IN}/A} = \frac{T_s}{V_C} \Rightarrow 1-D = \frac{V_{IN}/A}{V_C} \Leftrightarrow D = 1 - \frac{V_{IN}}{A \cdot V_C}$$



d) Calculate the voltage divider ratio A. $A = \frac{V_O}{V_C} = \frac{50}{5} = 10$

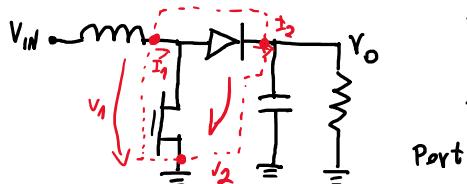
2a) Derive the line-to-output (audiosusceptibility) and the control-to-duty cycle transfer functions for a standard boost converter (no feedforward).

Apply small perturbations \tilde{v}_c and \tilde{v}_{IN} to V_C and V_{IN} respectively.

b) Calculate \tilde{d} as a function of \tilde{v}_c and \tilde{v}_{IN} .

c) Derive the control-to-output transfer function $G_{OC_{F.F.}}(s) = \frac{\tilde{V}_O(s)}{\tilde{V}_C(s)}$.

d) Derive the line-to-output transfer function $G_{OL_{F.F.}}(s) = \frac{\tilde{V}_O(s)}{\tilde{V}_{IN}(s)}$.



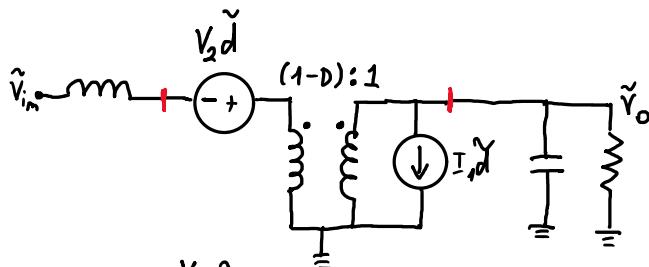
$$V_1(t) = V_2(1-q(t)) \Rightarrow \langle V_1 \rangle \approx \langle V_2 \rangle (1-d(t))$$

$$I_2(t) = I_1(1-q(t)) \Rightarrow \langle I_2 \rangle \approx \langle I_1 \rangle (1-d(t))$$

$$V_1 + \tilde{V}_1 = (V_2 + \tilde{V}_2)(1-D-\tilde{d}) \Rightarrow \begin{cases} V_1 = V_2(1-D) \\ \tilde{V}_1 = -V_2\tilde{d} + \tilde{V}_2(1-D) \end{cases}$$

$$I_2 + \tilde{I}_2 = (I_1 + \tilde{I}_1)(1-D-\tilde{d}) \Rightarrow \begin{cases} I_2 = I_1(1-D) \\ \tilde{I}_2 = -I_1\tilde{d} + \tilde{I}_1(1-D) \end{cases}$$

$$\begin{cases} V_1 = V_2(1-D) \\ \tilde{V}_1 = -V_2\tilde{d} + \tilde{V}_2(1-D) \end{cases}$$

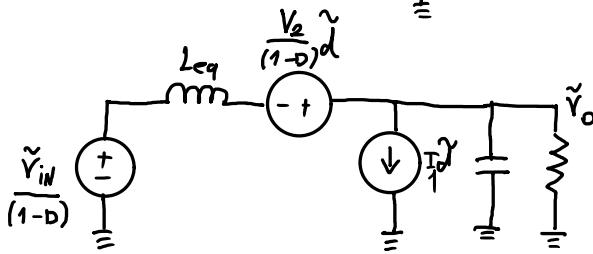


$$\frac{V_D}{V_{IN}} = \frac{1}{1-D}$$

$$V_2 = V_0$$

$$I_1 = I_{im} = I_0 \left(\frac{1}{1-D} \right)$$

$$L_{eq} = \frac{L}{(1-b)^2}$$



$$G_{0d} = \frac{\tilde{V}_0}{\tilde{d}} \Big|_{\tilde{V}_{im}=0, \tilde{I}_{im}=0}$$

$$G_{0l} = \frac{\tilde{V}_0}{\tilde{V}_{in}} \Big|_{\tilde{d}=0}$$

$$G_{0L} : \quad \text{Circuit diagram showing } G_{0L} \text{ as the ratio of } \tilde{V}_0 \text{ to } \tilde{V}_{in} \text{ through the load branch.}$$

$$R//C = \left(\frac{1}{R} + j\omega C \right)^{-1} = \frac{R}{1 + \Delta RC}$$

$$\tilde{V}_0 = \frac{R}{R + \Delta L_{eq}} \cdot \frac{\tilde{V}_{im}}{(1-D)} \Leftrightarrow \frac{\tilde{V}_0}{\tilde{V}_{im}} = \frac{1}{1-D} \cdot \frac{R}{R + \Delta L_{eq}(1 + \Delta RC)} =$$

$$\omega_0 = \frac{1}{\sqrt{C L_{eq}}}$$

$$= \frac{1}{(1-D)} \cdot \frac{1}{1 + \Delta \frac{L_{eq}}{R} + \Delta^2 C L_{eq}} = \frac{1}{1-D} \cdot \frac{1}{1 + \frac{1}{Q} \frac{\Delta}{\omega_0} + \frac{\Delta^2}{\omega_0^2}} \quad \frac{1}{Q} \cdot \frac{1}{\omega_0} = \frac{L_{eq}}{R} \Leftrightarrow Q = R \sqrt{\frac{C}{L_{eq}}}$$

$$L_{eq} = \frac{L}{(1-b)^2}$$

$$G_{0D} : \quad \text{Circuit diagram showing } G_{0D} \text{ as the ratio of } \tilde{V}_0 \text{ to } \tilde{d}.$$

$$G_{0D} = \frac{\tilde{V}_0}{\tilde{d}}$$

$$I_1 = I_{in} = \frac{V_{out}}{R} \cdot \frac{1}{1-D}$$

$$V_2 = V_{out}$$

$$\tilde{V}_0 \cdot \frac{1 + \Delta RC}{R} + \frac{V_{out}}{R} \cdot \frac{1}{1-D} \tilde{d} = \frac{(1-D)}{\Delta L_{eq}} \tilde{d} - \tilde{V}_0 \Leftrightarrow$$

$$\Leftrightarrow \tilde{V}_0 \left(\frac{1 + \Delta RC}{R} + \frac{1}{\Delta L_{eq}} \right) = \frac{V_{out}}{(1-D)} \cdot \left(\frac{1}{\Delta L_{eq}} - \frac{1}{R} \right) \tilde{d} \quad \omega_{RHPZ} = \frac{R}{L_{eq}}$$

$$\Leftrightarrow \frac{\tilde{V}_0}{\tilde{d}} = \frac{V_{out}}{(1-D)} \cdot \frac{\left(1 - \Delta \frac{L_{eq}}{R} \right)}{\Delta^2 L_{eq} C + \Delta \frac{L_{eq}}{R} + 1} = \frac{1 - \Delta \frac{1}{\omega_{RHPZ}}}{\frac{\Delta^2}{\omega_0^2} + \Delta \frac{1}{\omega_0} \frac{1}{Q} + 1}$$

$$\frac{V_{out} \cdot (1-D) V_C A}{(1-D) V_C^2} = \frac{V_{out}}{V_C} = A \quad V_{IN} = (1-D) V_C A \Rightarrow V_{IN} + \tilde{V}_{im} = (1-D - \tilde{d})(V_C + \tilde{V}_C) A$$

$$\begin{cases} V_{IN} = V_C A - D V_C A \\ \tilde{V}_{im} = \tilde{V}_C A - D \tilde{V}_C A - \tilde{d} V_C A \\ \tilde{d} = \frac{V_C A (1-D) - \tilde{V}_{im}}{V_C A} \end{cases}$$

$$G_{OC} = \frac{\tilde{V}_0}{\tilde{V}_C} = \frac{\tilde{V}_0}{\tilde{d}} \cdot \frac{\tilde{d}}{\tilde{V}_C} = \frac{V_{out}}{1-D} \cdot \frac{1 - \Delta \frac{1}{\omega_{RHPZ}}}{\frac{\Delta^2}{\omega_0^2} + \Delta \frac{1}{\omega_0} \frac{1}{Q} + 1} \cdot \frac{A \cdot V_C}{A \cdot V_C^2} =$$

$$A \cdot \frac{1 - \Delta \frac{1}{\omega_{RHPZ}}}{\frac{\Delta^2}{\omega_0^2} + \Delta \frac{1}{\omega_0} \frac{1}{Q} + 1} //$$

$$\tilde{d} = -\frac{1}{V_C A} \tilde{V}_{im} + \frac{V_{IN}}{A \cdot V_C^2} \tilde{V}_C$$

$$G_{0L} = G_{0d} \cdot \frac{\tilde{d}}{\tilde{V}_{im}} + G_{0L} = \frac{1}{\omega_0^2} G_{0L} = \frac{\Delta}{\omega_0^2} \cdot \frac{1}{1-D} \cdot \frac{1}{1 + \frac{1}{Q} \frac{\Delta}{\omega_0} + \frac{\Delta^2}{\omega_0^2}}$$