

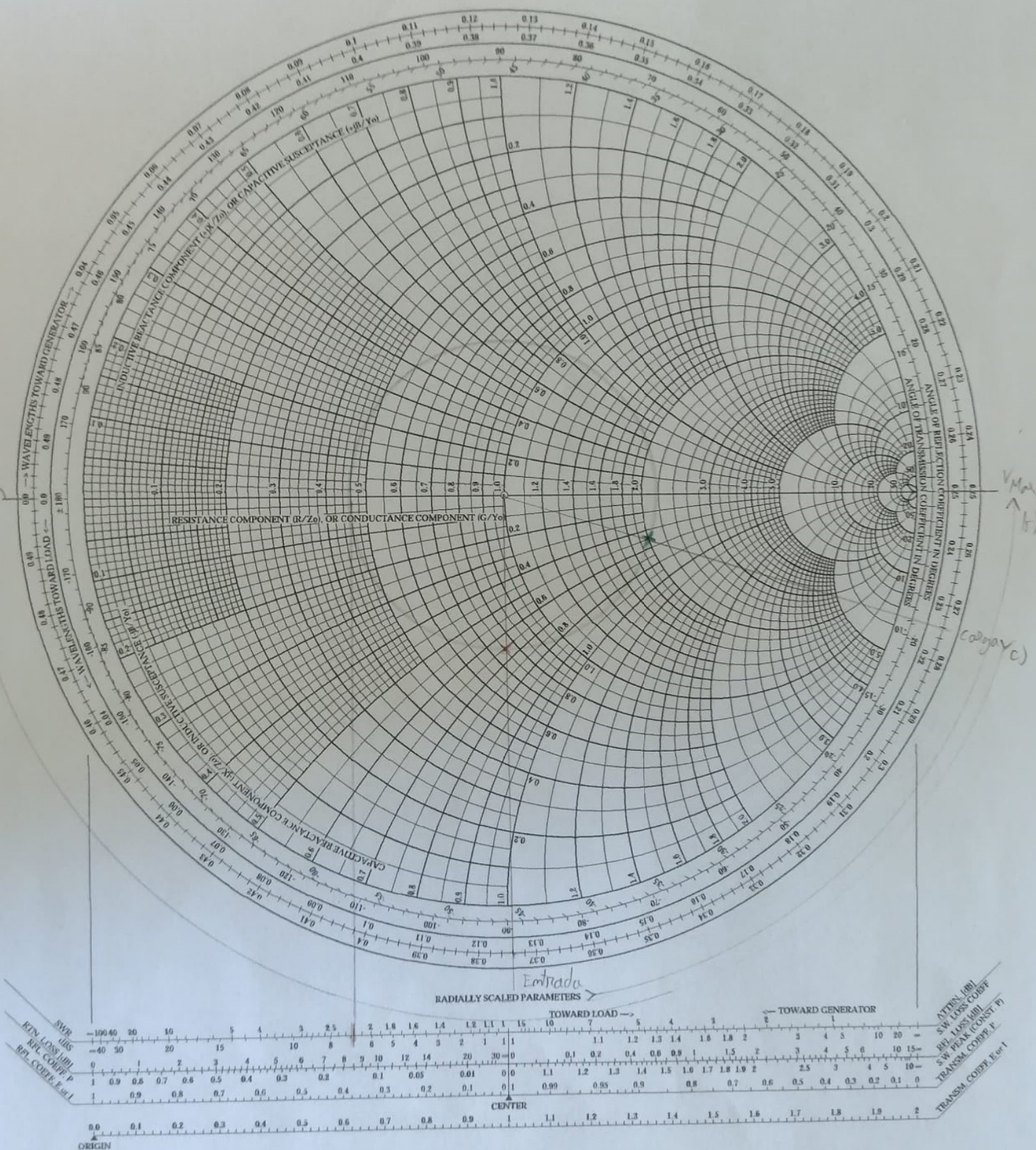
a) $0,75 - j0,65$

b) $0,374 - 0,25 \rightarrow 0,124\lambda$

c) $0,5 - j274 \rightarrow 0,226\lambda$

d) 2.2

The Complete Smith Chart



2) $Z_0 = 50 \Omega$ $Z_L = 23 - j48 \Omega \Rightarrow \eta_L = 0.46 - 0.90j$

a) $0.62 \angle -88^\circ = K_V$

$4.4 = \text{SWR}$

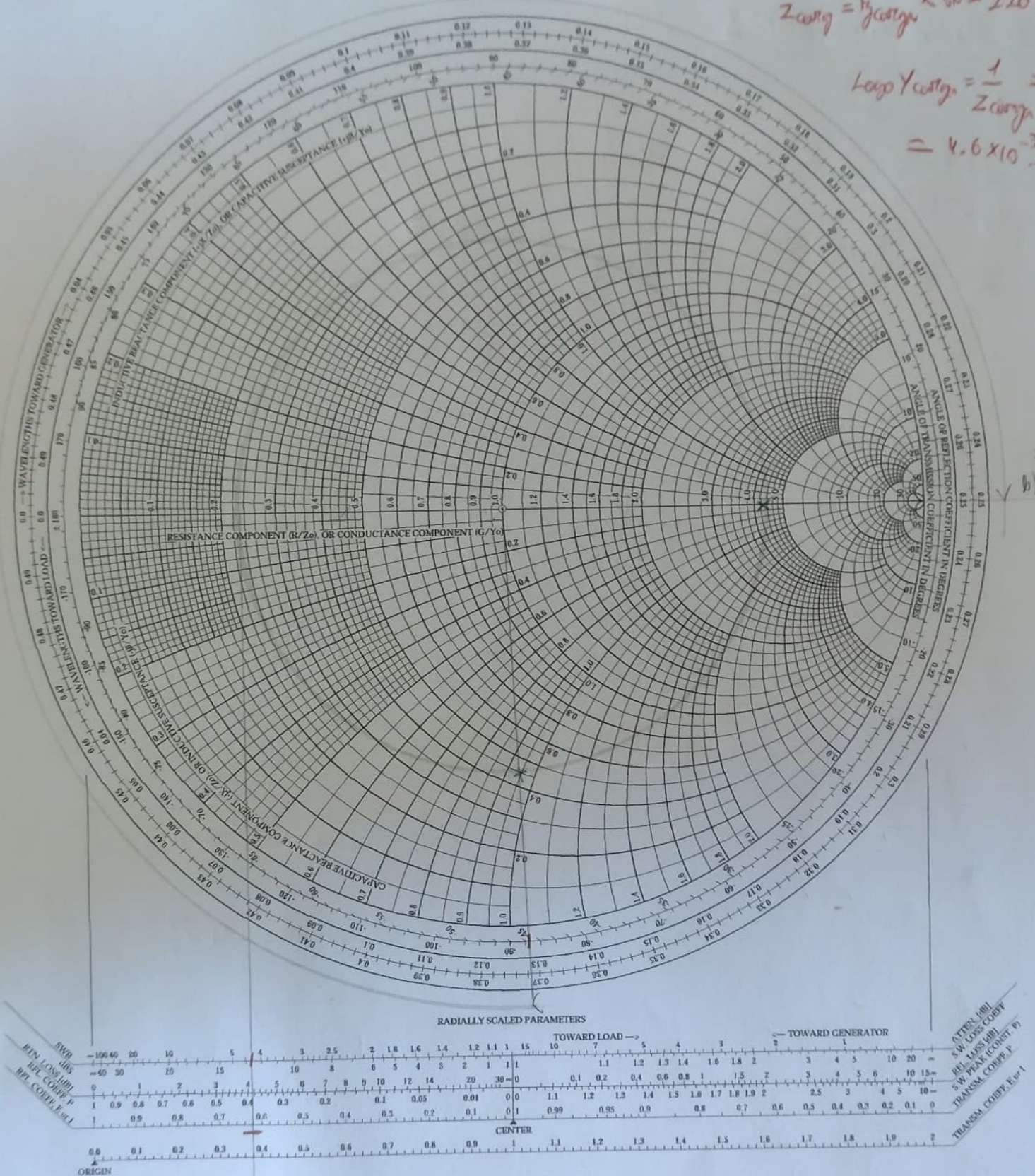
b) $0.5 - (0.25 - 0.128j) = 0.25 + 0.128j \rightarrow 0.378 \lambda \rightarrow 0.945 \text{ m}$

The Complete Smith Chart

c) $l = 3.45 \text{ m} \rightarrow 1.38 \lambda \Rightarrow Z_{\text{cable}} \text{ no axial loading} \Rightarrow Z_{\text{cable}} = \text{SWR} = 4.4 \Omega$

$Z_{\text{cable}} = Y_{\text{cable}} \times 50 = 220 \Omega$

$\text{Loss } Y_{\text{cable}} = \frac{1}{Z_{\text{cable}}} = 4.6 \times 10^{-3} \Omega^{-1}$



3) $Z_0 = 50 \Omega$

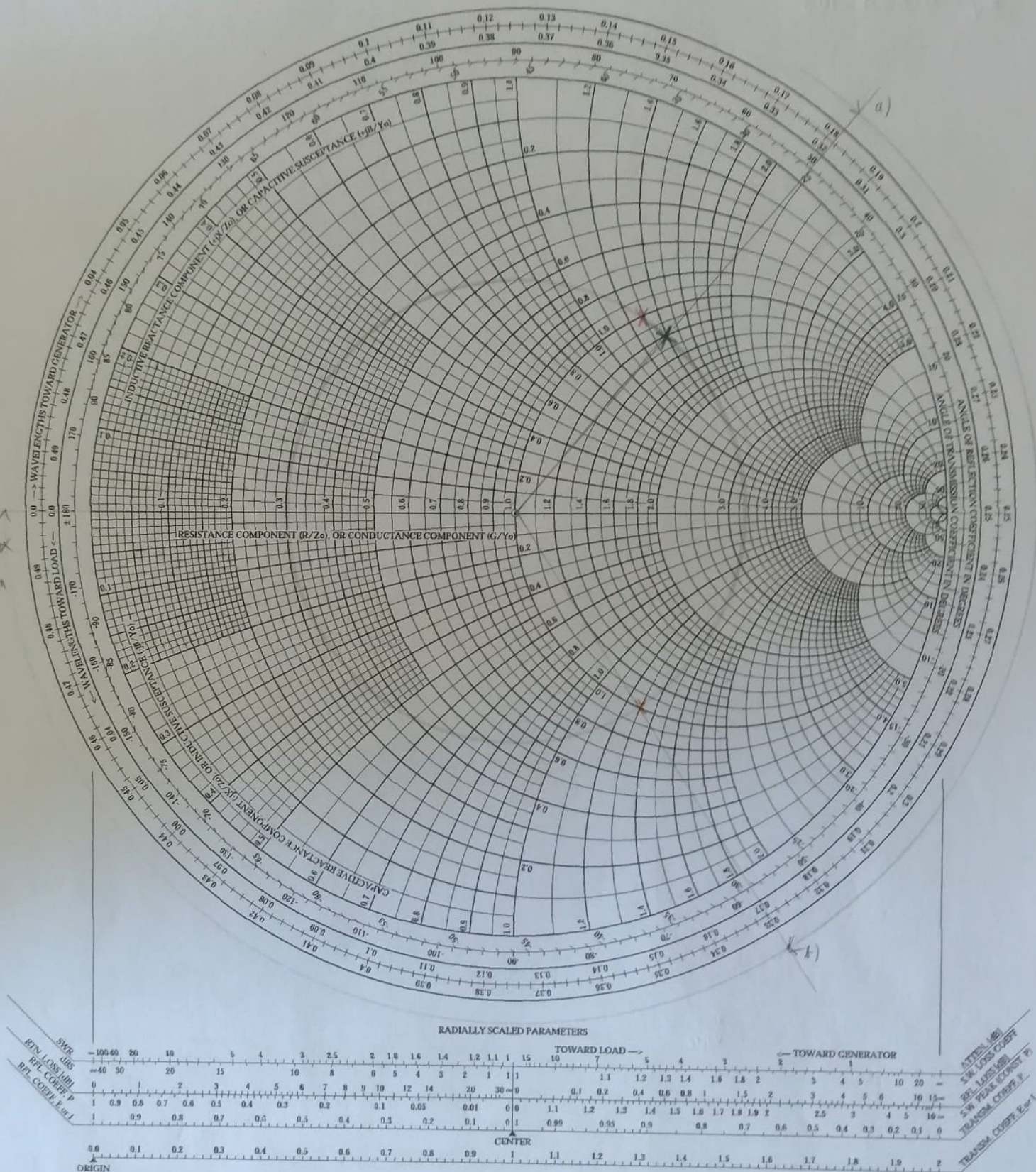
$\gamma_L = 1.2 + j1.4$

1) $0.5 - (0.182) = 0.318\lambda \Rightarrow 25.44 \text{ cm}$

2) $0.33 - 0.182 = 0.148\lambda \Rightarrow 11.84 \text{ cm}$

The Complete Smith Chart

Use como carta de admitância!



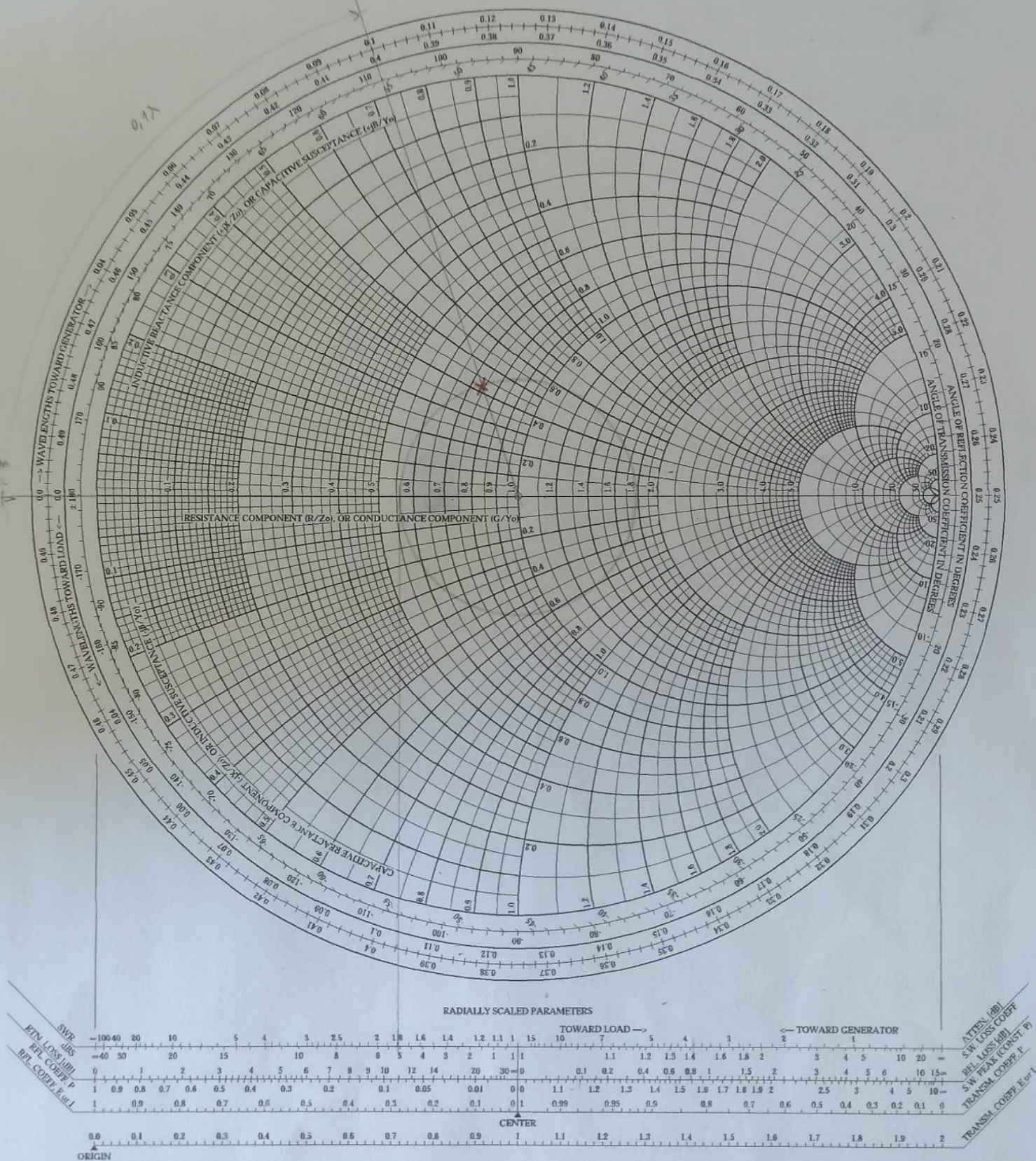
4) $\Gamma_{WR} = 1.8$

$Z_0 = 50$

$\lambda = 80 \text{ cm}$

$\Gamma_L = 0.74 + 0.44j$

The Complete Smith Chart



5) a) $27 - 12 = 15 = \frac{\lambda}{2} \Rightarrow \lambda = 30 \text{ cm}$

b) $c = \lambda f \Leftrightarrow f = \frac{c}{\lambda} = 10 \times 10^8 \text{ Hz} \Rightarrow 10 \text{ GHz}$

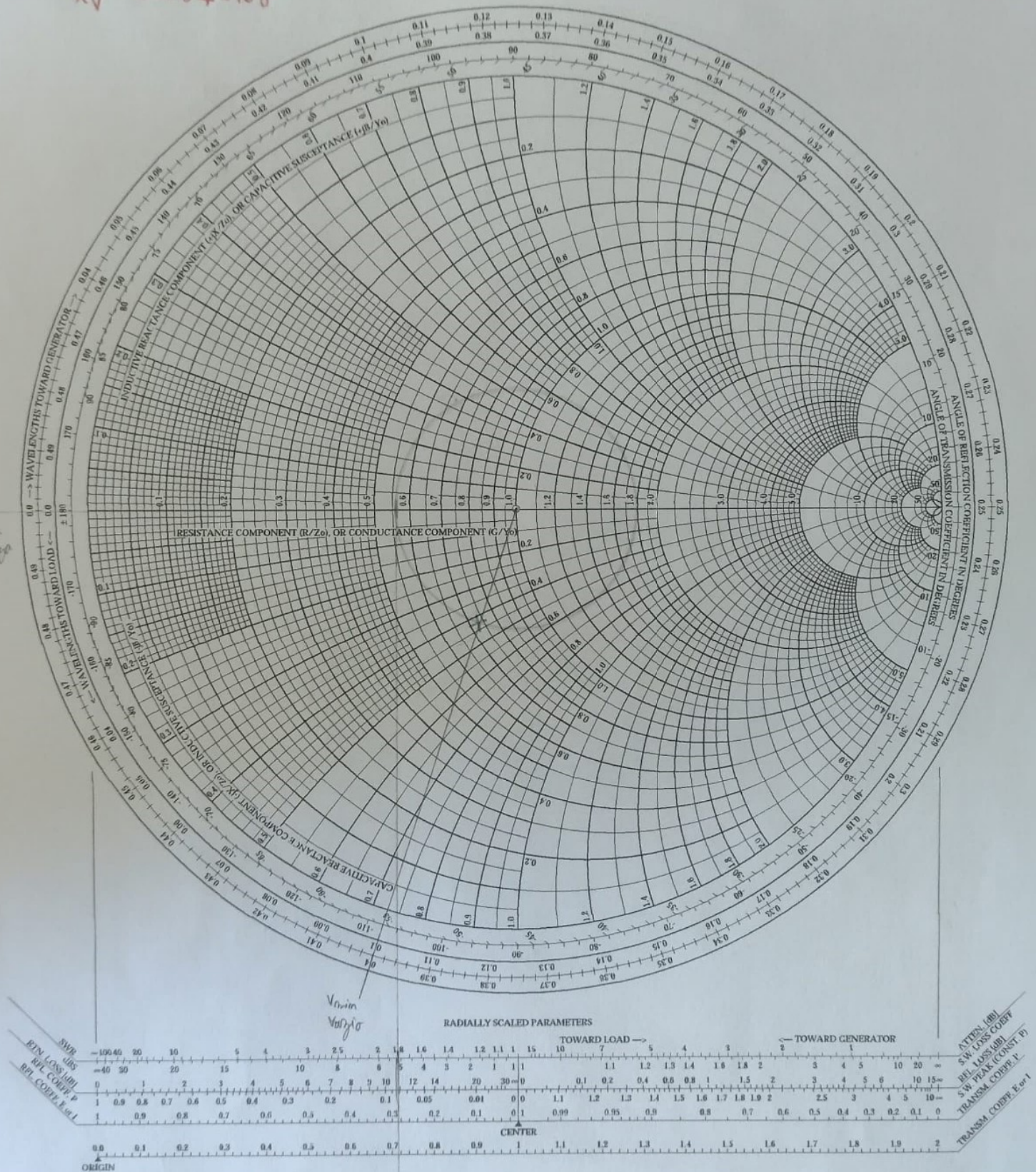
c) $\text{SWR} = \frac{0.72}{0.4} = 1.8$

d) $0.725 - j0.42$

Coax - 9 cm $\rightarrow 0.3\lambda$
CC - 12 cm $\rightarrow 0.4\lambda \rightarrow 0.1\lambda$

The Complete Smith Chart

$K_V = 0.284 \times 108^\circ$



6) a) $c = f\lambda \Leftrightarrow \lambda = \frac{2}{3}c_0 = 20 \text{ m}$

b) $\gamma_L = 2 + j2$ (x)
 $\gamma_L = 1 - j1$ (o)

Minor $l_{se} \Rightarrow \text{outside } 1$

Large $l_1 = 0.22\lambda$

c) $l_{se1} = 0.089\lambda$

$b_1 = 1.6$

$b_{stab1} = -b_1 \Leftrightarrow \text{catalang}(\beta l_{st1}) = b_1 \Leftrightarrow l_{se1} = 0.089\lambda$

$l_1 = 0.22\lambda$

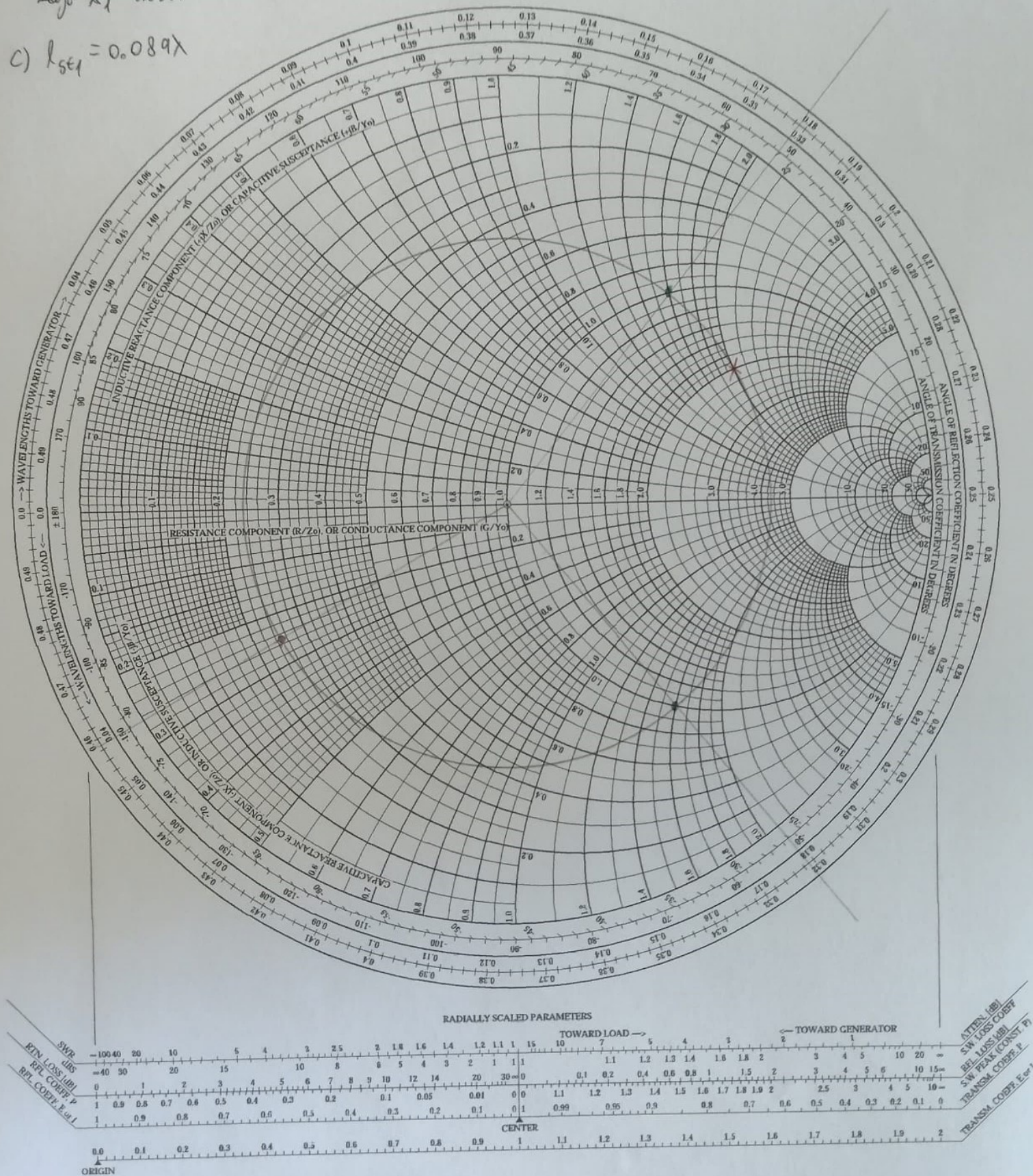
or $l_2 = 0.362\lambda$

$b_{stab2} = -b_2 \Leftrightarrow \text{catalang}(\beta l_{st2}) = b_2 \Leftrightarrow l_{st2} = 0.41\lambda$

The Complete Smith Chart

$b_2 = -1.6$

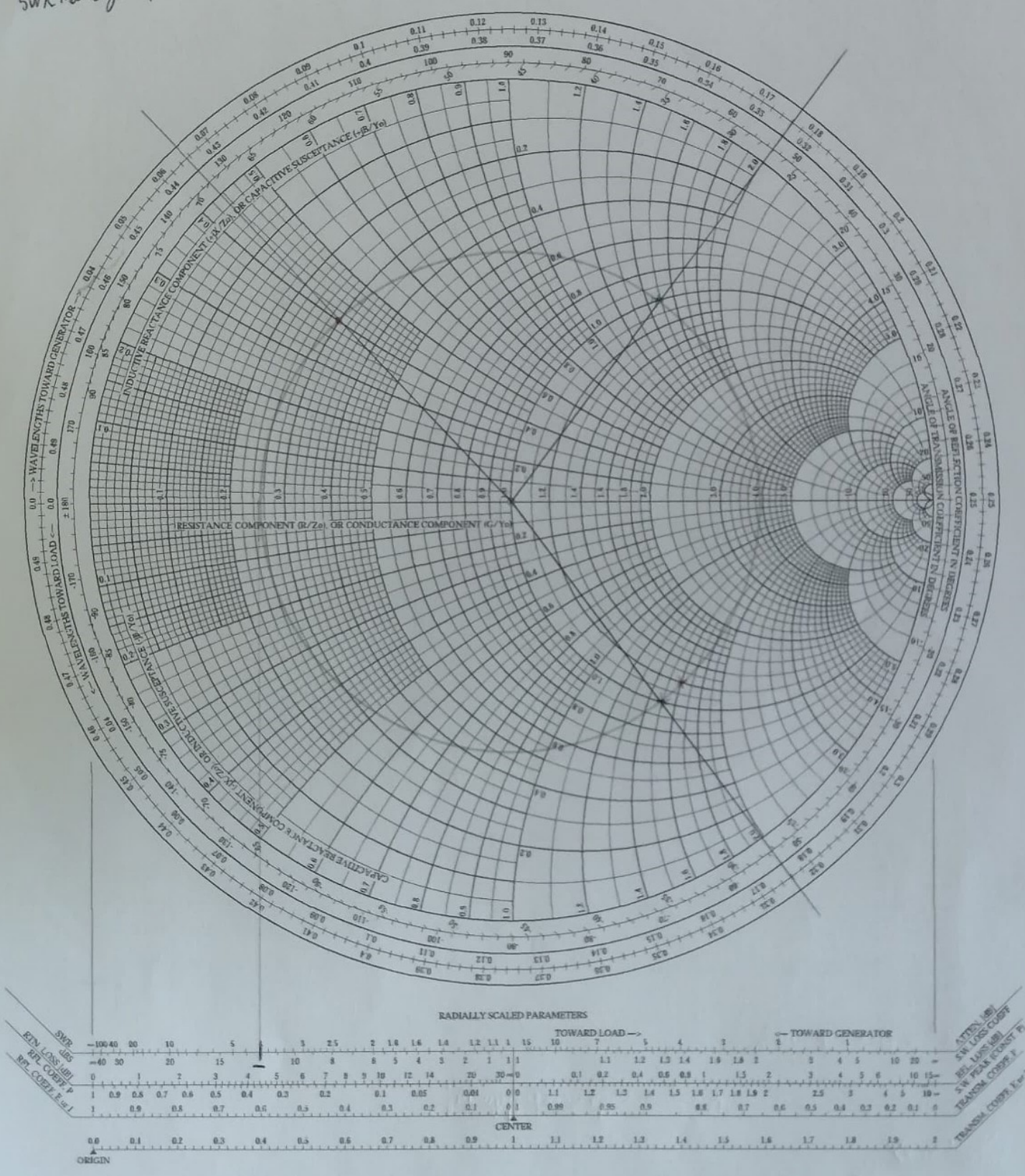
$R_2 \gamma_{im} \gamma = 1$



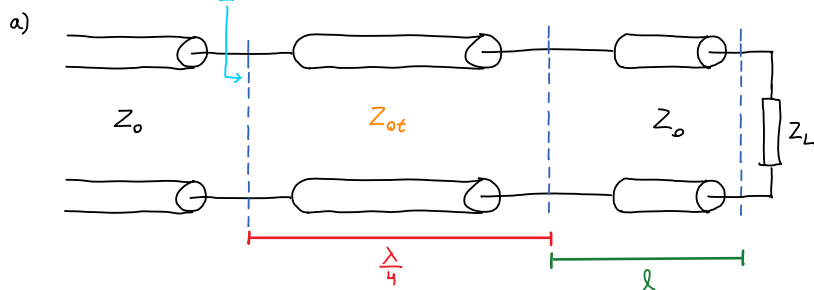
$\lambda = 1$
 $\gamma_L = 1.2 + j1.6$ (x)
 $\gamma_L = 0.3 + j0.4$ (o)
 a) $\Gamma_1 = 0.111\lambda \rightarrow b_1 = 1.5 \rightarrow \cotang(B)\Gamma_{st1} = b_1 \Leftrightarrow \Gamma_{st1} = 0.094\lambda$
 $\Gamma_2 = 0.259\lambda \rightarrow b_2 = -1.5 \rightarrow \cotang(B)\Gamma_{st2} = b_2 \Leftrightarrow \Gamma_{st2} = 0.41\lambda$
 Nullen auf $\Gamma = 0 \rightarrow \Gamma_1 = 0.11\lambda \quad \Gamma_{st1} = 0.094\lambda$

b) SWR max Anta: 1
 SWR max Stat: ∞ (E-M C.C.)
 SWR max Geop: 4

The Complete Smith Chart



8)



$$Z_L \text{ é real } (Z_L = 100 \Omega) \Rightarrow l = 0$$

$$\text{Queremos: } Z = Z_0$$

$$\text{Logo } \frac{Z_{0e}^2}{Z_L} = Z \Leftrightarrow Z_{0e} = \sqrt{Z_0 Z_L} = \sqrt{5000} \approx 70.7 \Omega$$

$$b) \text{ Linha adaptado } \Rightarrow SWR = 1$$

$$c) f = 1.6 \text{ GHz} \quad c = \lambda^* f^* \Leftrightarrow \lambda f = \lambda^* f^* \Leftrightarrow \lambda = 1.1 \lambda^*$$

$$f^* = 1.1 \text{ GHz}$$

$$\text{Como } f \neq 1.6 \text{ GHz} \Rightarrow Z^* \neq Z_0 \Rightarrow \text{Não está adaptado}$$

$$Z^* = Z_{0e} \frac{Z_L + j Z_{0e} \tan(\beta \frac{\lambda}{4})}{Z_{0e} + j Z_L \tan(\beta \frac{\lambda}{4})} = 50.92 e^{0.109j} \Omega$$

$$\beta \frac{\lambda}{4} = \frac{2\pi}{\lambda^*} \frac{\lambda}{4} = \frac{1.1\pi}{2}$$

$$K_V = \frac{Z^* - Z_0}{Z^* + Z_0} \Rightarrow |K_V| = 0.055$$

$$SWR = \frac{1 + |K_V|}{1 - |K_V|} = 1.117$$